

The EFO Officers

2014

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The Next Flying Meeting: Sat., June 14, 10 a.m., Midwest RC Society 7 Mi. Flying Field

What's In This Issue:

Part 2: An Initial Safe Center of Gravity (ISCG); Using the Mean Aerodynamic Chord (MAC) and Aerodynamic Center (AC) - 80" Span Eindecker -Upcoming Keith Shaw Birthday Party Electric Fly-in 2014 - Announcing the 30th Annual Mid-America Electric Flies - Upcoming Events

> Part 1 ended with the following: "The calculated semispan mean chord of the two panels was added by the author to Mr. Diehl's illustration and is shown in red. Note that the average mean chord of the semispan is NOT the MAC, according to Mr. Diehl. What happened?"

Part 2

On page 415 of Mr. Diehl's report, he states, "There is a definite forward shift in the aerodynamic center of a wing due to the addition of a fuselage or of nacelles." He explained how to calculate the forward shift of the AC because of the influence of the fuselage and nacelles, when present. His calculations included the the placement



of the wing on the fuselage, when referenced from the fuselage axis, as well as the length of the fuselage. For modeling purposes, his process is much too complicated. It is most important to note that there is a forward shift of the AC when a fuselage is added to a wing. The forward shift of the AC results in the actual MAC not being the semispan's mean chord.

On page 418 of the report he also noted, "Failure to allow for this shift will lead the designer to locate the airplane center of gravity too far aft."

A practical solution, that works for his illustration, should be good enough for a model aircraft.

The illustration shows that the Aerodynamic Center (AC) has moved forward on the semispan's mean chord to a position that is 19.3% of the semispan's median chord. The result is that the actual Mean Aerodynamic Chord (MAC) is shifted towards the root chord for this example. The chord of the illustration's actual MAC becomes (mean chord-(mean chord*.193))/0.75, or (2.6654-(2.6654*0.193))/0.75=2.8679. The AC is 2.8679/4=0.717 on the MAC and the MAC's distance is 3.854" from the root chord, as measured on the CAD drawing.

The AC shift is only part of the solution for deriving an ISCG. The horizontal stabilizer's area and the distance from the wing's AC to the horizontal stabilizer's AC, its tail moment, also influence the CG placement. The neutral point must also be taken into consideration.

From previously quoted sources, "Placing CG 5% - 15% of MAC in front of NP creates a longitudinal (pitch) stability called Static Margin. A lower margin (tail heavy) produces less stability and greater elevator authority, while a higher margin (nose heavy) creates more stability and less elevator authority. Too high of a static margin results in elevator stall at take off and landing."

Calculating the neutral point

The Neutral Point as a percentage of the MAC = 0.25 + (0.25 * sqrt(sqrt(aspect ratio of the wing)) * (horizontal stabilizer area / wing area) * (Tail moment / MAC) http://chrusion.com/BJ7/SuperCalc7.html It should be noted that the validity of the above formula could not be confirmed. All other references to the formula appear to be circular. aspect ratio of the wing (ARw) = (wing semispan * 2) 2 / wing area

tail volume ratio aka (Vbar) with the result as a percentage = (horizontal stabilizer area / wing area) * (Tail moment / MAC)

A second spreadsheet was created in the Excel workbook to allow for the AC shift to become 25% of the shifted MAC.

http://www.theampeer.org/ampeer/ampmay14/ISCG.xls Using Data from the spreadsheet for the shifted

MAC, the CG formulas were reevaluated.

Wing Aspect Ratio (ARw) 10.56088 10.56088 Tail Moment Ratio (Vbar) 0.63430 0.59492 Neutral Point (NP) as % of chord 53.59% 51.81% Distance from leading edge (LE) of chord to NP 4.42691 4.60562 Distance from NP to Aerodynamic Center (AC) 2.36159 2.38334 Percent of chord between NP and AC 28.59% 26.81% Distance from Rot Chord LE to NP 5.76563 5.31648 Static Margin 5% LE chord to Center of Gravity (CG) 4.01385 4.16117 Distance from Root Chord LE to CG 5.35256 4.87202 Static Margin 5% as % of chord 48.59% 46.81% Static Margin 15% LE chord to CG 3.18772 3.27225 Distance from Root Chord LE to CG 4.5643 3.98311 Static Margin 15% as % of chord 38.59% 36.81% Static Margin 20% LE chord to CG 2.77466 2.82779 Distance from Root Chord LE to CG 4.11337 3.53865 Static Margin 20% as % of chord 33.59% 31.81% For Comparison: 4.611337 3.80701 <	Sea Ranger	Mean Chord	Shifted MAC
Tail Moment Ratio (Vbar) 0.63430 0.59492 Neutral Point (NP) as % of chord 53.59% 51.81% Distance from leading edge (LE) of chord to NP 4.42691 4.60562 Distance from NP to Aerodynamic Center (AC) 2.36159 2.38334 Percent of chord between NP and AC 28.59% 26.81% Distance from Rot Chord LE to NP 5.76563 5.31648 Static Margin 5% LE chord to Center of Gravity (CG) 4.01385 4.16117 Distance from Root Chord LE to CG 5.35256 4.87202 Static Margin 5% as % of chord 48.59% 46.81% Static Margin 15% LE chord to CG 3.18772 3.27225 Distance from Root Chord LE to CG 4.52643 3.98311 Static Margin 20% LE chord to CG 2.77466 2.82779 Distance from Root Chord LE to CG 4.11337 3.53865 Static Margin 20% as % of chord 33.59% 31.81% For Comparison: Van Putte: Distance from Root Chord LE to CG 4.32461 3.80701 Van Putte: Distance from Root Chord LE to CG 4.681% 34.83% Whitehead: Distance from Root Chor	Wing Aspect Ratio (ARw)	10.56088	10.56088
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Distance from leading edge (LE) of chord to NP 4.42691 4.60562 Distance from NP to Aerodynamic Center (AC) 2.36159 2.38334 Percent of chord between NP and AC 28.59% 26.81% Distance from Root Chord LE to NP 5.76563 5.31648 Static Margin 5% LE chord to Center of Gravity (CG) 4.01385 4.16117 Distance from Root Chord LE to CG 5.35256 4.87202 Static Margin 15% as % of chord 48.59% 46.81% Static Margin 15% as % of chord 3.8772 3.27225 Distance from Root Chord LE to CG 4.52643 3.98311 Static Margin 15% as % of chord 38.59% 36.81% Static Margin 20% LE chord to CG 2.77466 2.82779 Distance from Root Chord LE to CG 4.11337 3.53865 Static Margin 20% as % of chord 33.59% 31.81% For Comparison: 50 50 50 Van Putte: Distance from Root Chord LE to CG 4.32461 3.80701 Van Putte: Distance from Root Chord LE to CG 4.32461 3.80701 Van Putte: Distance from Root Chord LE to CG 4.6	Neutral Point (NP) as % of chord	53.59%	51.81%
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Percent of chord between NP and AC 28.59% 26.81% Distance from Root Chord LE to NP 5.76563 5.31648 Static Margin 5% LE chord to Center of Gravity (CG) 4.01385 4.16117 Distance from Root Chord LE to CG 5.35256 4.87202 Static Margin 5% as % of chord 48.59% 46.81% Static Margin 15% LE chord to CG 3.18772 3.27225 Distance from Root Chord LE to CG 4.52643 3.98311 Static Margin 15% as % of chord 38.59% 36.81% Static Margin 20% LE chord to CG 2.77466 2.82779 Distance from Root Chord LE to CG 4.11337 3.53865 Static Margin 20% as % of chord 33.59% 31.81% For Comparison: 500 500 500 Van Putte: Distance from Root Chord LE to CG 4.32461 3.80701 Van Putte: Distance from Root Chord LE to CG 4.68063 4.17551 Whitehead: Distance from Root Chord LE to CG 4.68063 4.17551	Distance from NP to Aerodynamic Center (AC)	2.36159	2.38334
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Static Margin 5% as % of chord 48.59% 46.81% Static Margin 15% LE chord to CG 3.18772 3.27225 Distance from Root Chord LE to CG 4.52643 3.98311 Static Margin 15% as % of chord 38.59% 36.81% Static Margin 20% LE chord to CG 2.77466 2.82779 Distance from Root Chord LE to CG 4.11337 3.53865 Static Margin 20% as % of chord 33.59% 31.81% For Comparison: Van Putte: Distance from Root Chord LE to CG 4.32461 3.80701 Van Putte: Distance from Root Chord LE to CG 4.68063 4.17551 Whitehead: Distance from Root Chord LE to CG 4.68063 4.17551	Distance from Root Chord LE to CG	5.35256	4.87202
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Whitehead: Distance from Root Chord LE to CG 4.68063 4.17551 Whitehead: % of chord 40 45% 38 98%	Van Putte: % of chord	36.14%	34.83%
Whitehead: % of chord 40 45% 38 98%	Whitehead: Distance from Root Chord LE to CG	4.68063	4.17551
Winterlead. // of offord 40.40/10 00.00/1	Whitehead: % of chord	40.45%	38.98%

A table was created to compare the data for the Sea Ranger's semispan mean chord to the same data for the shifted MAC of the Sea Ranger. Data was included in the table to compare the Van Putte and Whitehead formulas.

While a static margin of between 5% and 15% of the MAC was stated as 'typical' for CG placement, a static margin of 20% was added to the table for analytical purposes and to see if it might suggest a useable ISCG.

The Van Putte result of 36.14% of the mean chord is a static margin of 17.44%. The Whitehead result of 40.45% of the mean chord is a static margin of 13.13%. The Van Putte result of 34.83% of the shifted MAC is a static margin of 16.98% The Whitehead results of 38.98% of the shifted MAC is a static margin of 12.84%.

When the neutral point and static margins based on a percentage of the mean chord or shifted MAC

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are compared with the Van Putte and Whitehead formulas, the static margins appear to fall into the 'normal' range, but the the AC as a percentage of the mean or shifted MAC appears to be 'high' when compared to traditional percentages, 25% to 33%.

The Thunder Tiger Lazy Tiger Cub, An Atypical Design



The Thunder Tiger Lazy Tiger Cub is a very atypical RC design. It has a low aspect ratio wing and a relatively short tail moment and low tail volume ratio.

Before the first flight, the Lazy Tiger Cub's CG was checked and found to be near the manufacturer's rearmost suggested CG. It was at 3-3/4" from the wing's leading edge (LE) or 27.8% of the mean chord. According to the Thunder Tiger instruction manual, "Your Lazy Tiger Cub should balance 3-1/2" (26% of 13.5" chord) to 3-3/4" (28% of chord) back from the leading edge of the wing (about 3/8" in front of the main spar.)" At the time, that seemed to make sense as the percentage fell within the 'typical' range.

The first flight did not go well. There were several 'issues' with the plane. One of the 'issues' was definitely the CG. It was extremely pitch sensitive and almost uncontrollable. A CG dive test was performed. The plane started a 1/2 outside loop during the dive test. The CG dive test indicated that it was extremely tail heavy.

The CG Dive Test:

A How To and What the Results Mean

How: (It is best to do this test on a close to windless day and into the wind. It must be performed so that observations can be made as to what is happening.)

 Trim the plane for level flight at cruising speed
Once the plane is trimmed, while flying level at cruising speed, push the nose down into a 30-deg to 40-deg dive without changing the motor/engine speed

3. Once the plane is descending in a straight line down the angle, let go of the elevator stick

- 4. Watch what happens
- 5. Repeat the process a few times



What the observations mean:

1. If the plane continues in a straight line, it is neutrally stable

2. If the plane pulls up, it is nose-heavy

3. If the plane increases its downward angle or even 'tucks under', the plane is tail-heavy

For more information on the CG Dive Test see Keith Shaw's "The Art of Low Power Aerobatics". http://www.theampeer.org/shaw/aerobat.pdf

To get the 'Cub' to fly well, and not be overly pitch sensitive, the CG was eventually moved to approximately 1-3/4" from the leading edge of the wing. It remains at that point and has been used as the "club" trainer for years. The CG position is approximately 13% of the mean chord.

Required measurements for the spreadsheet input for the Lazy Tiger Cub.

Wing:

Root and Tip Chord: 13.5" Leading Edge Sweep: 0"

Span: 50"

Horizontal Stabilizer:

Root Chord: 6.813" Tip Chord: 3.407" Leading Edge Sweep: 2.219" Span: 8.75"

Wing Root Chord LE to Horizontal Stabilizer Root Chord LE: 23.875"

Thunder Tiger Lazy Tiger Cub	Mean Chord	Shifted MAC
Wing Aspect Ratio (ARw)	3.7037	3.7037
Tail Moment Ratio (Vbar)	0.22385	0.22982
Neutral Point (NP) as % of chord	32.76%	32.97%
Distance from leading edge (LE) of chord to NP	4.42309	4.45102
Distance from NP to Aerodynamic Center (AC)	1.048092	1.84552
Percent of chord between NP and AC	7.76%	13.67%
Distance from Root Chord LE to NP	4.42309	4.45102
Static Margin 5% LE chord to Center of Gravity (CG)	3.74809	3.77602
Distance from Root Chord LE to CG	3.74809	3.77602
Static Margin 5% as % of chord	27.76%	27.97%
Static Margin 15% LE chord to CG)	2.39809	2.42602
Distance from Root Chord LE to CG	2.39809	2.42602
Static Margin 15% as % of chord	17.76%	17.97%
Static Margin 20% LE chord to CG	1.72309	1.75102
Distance from Root Chord LE to CG	1.72309	1.75102
Static Margin 20% as % of chord	12.76%	12.97%
For Comparison:		
Van Putte: Distance from Root Chord LE to CG	3.03235	2.28969
Van Putte: % of chord	22.46%	16.96%
Whitehead: Distance from Root Chord LE to CG	3.38327	3.41346
Whitehead: % of chord	25.06%	25.28%

A table was created for the Lazy Tiger Cub that compared the semispan's mean chord, semispan's **shifted** MAC, Van Putte's formula and Whitehead's formula.

The table illustrates that using a static margin of 15%, for either the mean chord or shifted MAC, to select the ISCG for the Lazy Tiger Cub, the first flights **would not** have resulted in an overly pitch sensitive aircraft. It also indicates that when the Van Putte formula is used with the shifted MAC spreadsheet data, the recommended CG could also be an ISCG.

The table also illustrates that the Whitehead formula does not provided a useful ISCG no matter whether the mean chord or shifted MAC data was used.

A table was created, shown at the bottom of the page, using the proposed Japanese 'Judy' bomber from Mr. Irving's article, the Sea Ranger and the Lazy Tiger Cub. The Whitehead formula was eliminated from table as his results do not appear useful in selecting an ISCG. All three planes are somewhat atypical.

The Judy bomber has a trapezoidal semispan with a 'normal' range aspect ratio for this type of plane. It also has a trapezoidal horizontal stabilizer semispan with a fairly long tail moment yielding a relatively high tail volume ratio, Vbar.

The Sea Ranger has two panels in the semispan. One is rectangular and the other trapezoidal. It has a relatively high aspect ratio for this type of plane. It also has a trapezoidal horizontal stabilizer semispan with a fairly long tail moment, again yielding a relatively high tail volume ratio, Vbar.

The Thunder Tiger Lazy Tiger Cub has a 'low' aspect ratio, rectangular wing semispan, trapezoidal horizontal stabilizer semispan, comparatively short tail moment and very low Vbar.

The actual flying CG of the Lazy Tiger Cub is 1.75". If the CG of the Lazy Tiger Cub is placed rearward or 2-3/8" from leading edge, it creates a plane that is extremely pitch sensitive and almost unflyable.

Next, three actual models were used to verify ISCG calculations.

MiG-17, 3-panel, swept wing and swept trapezoidal horizontal stabilizer, Jim Young, wingspan 28", Jim's proposed CG is 2.5" ahead of the trailing edge of the wing where it meets the fuselage - model not flown at this time http://www.rcgroups.com/forums/showthread.php?t=2040946 **Special Note on the MiG-17:** RC Lander produced a MiG-17. The manual is here:

http://www.rclander.com/Files/%7Bb8fd0141-58b9-4c6fb06b-a8e13cf20dc4%7D/Mig-17%20Operational %20Manual.pdf

Their recommended CG is shown on page 18 of manual and coverts to about 4-3/8" measured on the root chord ahead of the trailing edge for Jim's version. That's an odd way to put it, but for this

	Mean	Shifted MAC	Mean	Shifted MAC	Mean	Shifted MAC
	Judy	Judy	Sea Ranger	Sea Ranger	Lazy Cub	Lazy Cub
SM 15%	31.79%	30.19%	38.59%	36.81%	17.76%	17.97%
LE Root to ISCG	4.99	4.74	4.53	3.98	2.40	2.43
ARw	5.12995	5.12995	10.56088	10.56088	3.70370	3.70370
Vbar	0.57910	0.53672	0.63430	0.59492	0.22385	0.22982
Van Putte	34.30%	32.89%	36.14%	34.83%	22.46%	16.96%
VP LE Root to CG	5.29	5.08	4.32	3.81	3.03	2.29

model, using a reference point noted as ahead of the trailing edge works out well.

North American XP-51H forward swept wing and trapezoidal horizontal stabilizer, Mark Rittinger, wingspan 36", Mark's CG was noted as 2" in front of the leading edge at the wing root leading edge model flown successfully

http://www.rcgroups.com/forums/showthread.php?t=1664516 E-flite Extra 300 32e trapezoidal wing and horizontal stabilizer, Arthur Deane, wingspan 52.5", supplier recommended CG 3.5 - 3.875 in. back from LE closest to the fuse

http://www.e-fliterc.com/Products/Default.aspx?ProdID=EFL4125 A CAD drawing of an EXTRA 300,

dimensioned to the E-flite wingspan, showed that for both the mean chord and shifted MAC for the Eflite Extra 300 a static margin of 15% fell within Eflite's suggested CG range. The Van Putte formula, using the shifted MAC data, provided a CG recommendation that fell only slightly, less than 1/8", to the rear of the recommended CG range by E-flite.

The Swept Wing Conundrum

Both the MiG-17 and the proposed North American XP-51H have swept wings. The MiG's is a typical rearward sweep and the proposed XP-51H had a proposed forward sweep.

A CAD drawing of a MiG-17 was created. Both Jim's initial CG and the RC Lander recommended CG, scaled to Jim's 28" span, were noted on the drawing. The mean chord and shifted MAC were calculated using the spreadsheet. (Drawing on next page.)

The results were unexpected. The mean chord's neutral point (NP) was calculated to be ahead of the Lander and Jim's initial CG estimation.

To verify if something had gone wrong with the spreadsheet, the data was placed into the online calculator at http://adamone.rchomepage.com/ cg3_calc.htm.

Using a Static Margin (SM) of 15% the calculator showed a Mean Chord of 7.94", which was the same as the spreadsheet. The calculator calculated a NP slightly farther forward than the spreadsheet for the mean chord.

In post #54 of Mark Rittinger's build thread for his North American XP-51H he noted, "I made a 1/16 balsa glider to double check my CG calcs."



A reduced size glider of a MiG-17 was built using 1/8" balsa for the fuselage and 1/16" balsa for the wing and horizontal tail.

The CG was adjusted using various size screws taped to the front of the fuselage.

The initial CG was set at the AC suggest by the CAD drawing. The glider nosed into the ground after a very brief glide. The mean chord, and therefore the shifted MAC were NOT a very good ISCG as the glider was too nose heavy.

Adjustments were made to the CG to find the "best glide" without the model "pitching up" or "nosing in." The best "downhill" glide was found to be when the CG was located between 7/8" and 1" from the center section trailing edge. On the glider, the Lander recommended CG is located about 1" in front of the trailing edge.

A new formula was created and inserted into the shifted MAC spreadsheet to emulate the data found using the MiG-17 glider.

To verify the swept wing formula, a second swept wing glider was built using the plans from the July, 1934 Universal Model Airplane News. Article: http://www.theplanpage.com/how%20to %20articles/fundamentals%20of%20model%20airplane %20building/part%203/part%203.htm Plans: http://www.theplanpage.com/how%20to %20articles/fundamentals%20of%20model%20airplane %20building/part%203/Part%203%20p1.TIF

The model was built full size with a span of 15-1/8". A static margin of 15% of the reformulated shifted MAC spreadsheet provided an excellent



"downhill" gliding CG, which was 3/4" behind the

CG shown on the plans. When flown with the CG as marked on the plans, the plane was noticeably 'nose heavy'.



A double-size MiG-17 glider was created. The ISCG was calculated using the reformulated shifted MAC spreadsheet with a 15% static margin. The CG on the larger MiG-17 glider was adjusted to the recommended 15% static margin point. From the first toss, the glide was as expected.

A table (top of next page) was created to evaluate the ISCG for the three existing models. The dimensions were based on Internet 3-views and the wingspans stated by the designer or supplier. **Note:** The table indicates Leading Edge (LE) Root Chord distance to the ISCG, but for the MiG-17 that measure is from the trailing edge root chord to the ISCG.

As a final test for the shifted MAC spreadsheet, I used a 3-view of the Boeing Sea Ranger to create a 24.75" glider of the Sea Ranger. (Shown on the next page).

The glider was balanced using a 15% static margin at 1-3/16" behind the root leading edge, as suggested by the shifted MAC spreadsheet. The first toss across the basement was a nice 'downhill' glide. Just what I was looking for!

David's model data for the Sea Ranger was reentered into the shifted MAC spreadsheet.

He stated that he had decided to use 3.6" from the root leading edge as his initial CG.

The shifted MAC spreadsheet noted the CG was at 3.5" from the leading edge of the root chord

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	Mean	Shifted MAC	Mean	Shifted MAC	Mean	Shifted MAC
	MiG-17	MiG-17	NA XP-51H	NA XP-51H	Extra 300	Extra 300
SM 15%	22.68%	22.13%	27.92%	30.77%	32.86%	31.10%
LE Root to ISCG	6.14	3.79	-0.91	-1.63	4.06	3.92
ARw	3.68570	3.68570	5.10946	5.10946	5.33770	5.33770
Vbar	0.36603	0.35013	0.47676	0.55259	0.60150	0.55517
Van Putte	27.20%	26.67%	30.89%	33.42%	35.05%	33.51%
VP LE Root to CG	6.81	3.47	-0.67	-1.44	4.28	4.19



when using a 20% static margin and 4" from the root chord leading edge when a 15% static margin was used.

It looks like David's 3.6 inches from the root rib's leading edge falls within the range (15% to 20% static margin using the shifted MAC) for an initial safe CG.

Why All of This CG Information Overload?

With the CG usually marked on the plans or noted in the construction or assembly manual, why did I feel that it was necessary to devote two issues of the *Ampeer* to this topic?

In the January 2004 *Ampeer*, Keith Shaw noted, "There are many kits on the market that have the center of gravity in ridiculous spots and have incredible angles of attack. To them, if the plane flies, it's a good airplane. It really depends on what you want to do and what means something. If flying overhead with transparent covering is desired, then you can do anything. If super long flight times mean something, then that means efficiency."

http://www.theampeer.org/ampeer/ampjan04/ampjan04.htm#CG

In 2011, the Super Tiger Lazy Tiger Cub turned out to be the type of plane Keith was talking about. The first flight of that simple design almost ended as the last flight of that simple design because the recommended CG range was very wrong, and I was not knowledgable enough about CG to realize it.

Over the years I've run into several other airframes with 'uncomfortably' rearward CG recommended ranges by the manufacturer or supplier. Most recently they have included the parkzone T-28, E-Flite PT-17 and Maxford Antonov An-2. Luckily, the initial flights with them were successful enough to allow the CG to be tweaked to the pilot's ability and expectations as well as the plane's mission.

One way to do that tweaking, and the explanation for it, is in the previously noted Keith Shaw article in the January 2004 *Ampeer*.

Besides getting the CG right, it is important to have a good design based on solid aerodynamic principles.

The following are references for information regarding Reynolds Number, span efficiency and the Oswald's efficiency factor.

These are 'Word' documents, Search Google for: INTRODUCTION TO AERONAUTICS: A DESIGN PERSPECTIVE

CHAPTER 4: WINGS AND AIRPLANES and

ESTIMATING R/C MODEL AERODYNAMICS AND PERFORMANCE, Dr. Leland M. Nicolai, Technical Fellow, Lockheed Martin Aeronautical Company 2009 A Final Thought

If for some reason all of this math is too much for you, and you suspect that the recommended CG range might not be correct, take the time to make a glider of the model and give it a try.

Let's get that CG right BEFORE the first flight!

80" Span Eindecker From David Hipperson via email



I had been working for a while on a self-designed sport scale Curtiss Jenny but the urge came for a change just to provide a break. Two things gave impetus in that one, I had a set of plans for the Balsa USA 80 inch span Eindecker and two, a photo of an Eindecker replica in a copy of "Fighter Aircraft in Colour" by Bill Gunston. This aircraft was, apparently, used for movie work and has the advantages of having both ailerons as well as conventional tail and elevators.

No criticism of the Balsa USA version, which I'm sure is great but I wanted to make some changes. Among these were a lighter structure, two piece wings with working rigging, an all moving rudder together with a more realistic undercarriage and tail skid. This meant it was worth re-drawing the plans but I kept the wing section along with much of that structure plus the stock tailplane.

I aimed for an all up weight of eight pounds and felt that if I achieved that 5S would be more than sufficient. As a motor I chose the OS 5020-490 and I mated this to a Turnigy 16 X 7 wooden prop. The ESC is a Hyperion Titan 80 amp OPTO which is not really needed but I have several and the keep the ESC cool under the worst of conditions. The packs are two 5S 3200 in parallel and it seems as if I use about 20 - 25 amps under normal flight. These two packs balanced the aircraft exactly without resorting to any lead which was a bonus.

The structure went together very easily and the photos may show how basic it all is. Mostly it is 1/4 square balsa, balsa sheet and various thicknesses of ply. The joiners for the wings consisted of a very robust spruce main spar plus a 3/16 K&S wire rod plus matching brass tube to the rear. All of the rigging is via 60 pound coated fishing trace matched up with Du-Bro quick links. The cowl came from an old aluminum kettle and aluminum self adhesive 2" wide tape was used to cover the area between the cowl and cockpit. The Spandau gun from Williams Bros was a dummy on the original too. Mine was sprayed with dark grey metallic with licks of black. Covering is entirely white Oratex (Protex) which was then brush painted using artist acrylic. The 'red' is a home mixed match to the photo being mainly red and yellow to produce a very 'orangy' red. All of the markings are just hand drawn using either

brush or felt tip pens. Finally an aerosol can of satin fixer was sprayed over the whole thing which gave a perfect (to me) colour and look to the entire airframe.



(cont. on page 10)

Upcoming Keith Shaw Birthday Party Electric Fly-in 2014

The Balsa Butchers will once again be hosting the "Keith Shaw Birthday Party Electric Fly-In" at their field near Coldwater, MI. The event will take place on May 31 and June 1, 2014.

Contest Director: Dave Grife - E-mail: grifesd@yahoo.com or Phone: 517.279.8445

Please e-mail or call with any questions.

The Flying Field will be open Friday, May 30 for early arrivals

Saturday, May 31, hours are from 9 a.m. 'til 5 p.m. Sunday, June 1, hours are from 9 a.m. 'til 3 p.m. Landing Fee is \$15 for the weekend.



Directions: Quincy is approximately 4.5 miles east of I-69. Clizbe Road is approximately 1.6 miles east of Quincy. The Flying site is approximately 1.5 miles south of US-12 on the west side of Clizbe Road.

30th Annual Mid-America Electric Flies 2014 At the 7 Mile Road MRCS Field AMA Sanctioned Saturday, July 12 & Sunday, July 13 Hosted by the: Ann Arbor Falcons and Electric Flyers Only

Flying Site Provided by the: Midwest R/C Society

Contest Directors are:

Ken Myers phone (248) 669-8124 or kmyersefo@theampeer.org http://www.theampeer.org for updates & info Keith Shaw (734) 973-6309 Flying both days at the Midwest R/C Society Flying Field - 7 Mile Rd., Salem Twp., MI Registration: 9 A.M. both days Flying from 10 A.M. to 5 P.M. Sat. & 10 A.M. to 3 P.M. Sunday

Pilot Entry Fee \$15 a day or \$25 both days Parking Donation Requested from Spectators

Saturday's Awards Best Scale Most Beautiful Best Ducted Fan Best Sport Plane CD's Choice Sunday's Awards Best Scale Most Beautiful Best Mini-Electric Best Multi-motor CD's Choice

Planes Must Fly To Be Considered for Any Award Saturday's & Sunday's Awards: Plaques for 1st in each category

Open Flying Possible on Friday Night Flying Possible, Weather Permitting, Friday & Saturday Nights Refreshments available at the field both days.

remember available at the nora boar days.

Potluck picnic at the field on Saturday evening.

Come and join us for two days of fun and relaxed electric flying.

Come, Look, Listen, Learn - Fly Electric - Fly the Future!

Merchandise drawing for ALL entrants

To locate the Midwest R/C Society 7 Mile Rd. flying field, site of the 2013 Mid -America Electric Flies, look near top left corner of the map, where the star marks the spot, near Seven Mile Road and Currie Rd.

The field entrance is on the north side of Seven Mile Road about 1.6 Miles west of Currie Rd. Address: 7419 Seven Mile Road, Salem Twp, MI 48167 - numbers are on the fence.

Because of their convenient location and the easy drive to the flying field, the Comfort Suites and Holiday Inn Express in Wixom, MI have been added to the hotels' listing. They are only 10 miles northwest of the field and located near I-96 and Wixom Road. See the map-hotel .pdf for more details.

http://www.theampeer.org/map-hotels.pdf



Upcoming E-vents	(80" Span Eindecker Continued from page 8)
May 31 & June 1, Keith Shaw Birthday - full details in this issue	As it happened the Eindecker turned out at less than 8 pounds and so in flight it is a real treat. If wished it happily flies comfortably on ailerons and elevator and that big, all
June 6, 7 & 8, National Electric Fly-in (NEFI), Muncie, IN, info nefi.modelaircraft.org	moving, rudder is mighty powerful which is great for stall turns (hammer heads). I made a minor mistake during one take off where I'd inadvertently clicked into full rate on the
Saturday, June 14, EFO flying meeting, 10 a.m., Midwest RC Society 7 Mi. Rd. Flying Field, Everyone with an interest is welcome, proof of AMA membership required to fly	rudder and for a moment or two it was more than a bit squirrely but I got away with it. Landing is a cinch and is just a matter of aiming it in the right direction while
June 28 Skymasters Electric Fly-In and Night Fly. More info at the http://www.skymasters.org. 10 a.m., Potluck 6 p.m., night fly to midnight. Event Director: Pete Foss, email petefoss@skymasters.org	keeping a little throttle on to overcome the drag which is surprisingly high. I have to be honest and say I'm still getting used to it but I like it better every time I take the Eindecker out. So far I haven't needed to put in a single click of trim so something must have worked.
July 12 & 13, 30th Annual Mid-America Electric Flies - full details in this issue.	If any one has any questions I've missed I can be contacted via Ken Myers and I thank him for this newsletter and letting me put in my latest piece
August 16, NATIONAL MODEL AVIATION DAY CELEBRATION benefitting WOUNDED WARRIOR PROJECT, Ultimate Soccer Arenas, Pontiac, MI, 11 - 3, sponsored by MICHIGAN INTERNATIONAL AIRCRAFT ASSOCIATION, contact JOE HASS 248-321-7934	Regards David Hipperson Kilsyth, Victoria, Australia

The Ampeer/Ken Myers 1911 Bradshaw Ct. Commerce Twp., MI 48390

http://www.theampeer.org

The Next Monthly Flying Meeting: Date: Thursday, June 14, 2014 Time: 10 a.m. Place: Midwest RC Society 7 Mi. Rd. Flying Field